

第5章

基于LMI的控制系统抗饱和和控制

在实际的控制系统中,由于其自身的物理特性而引起的执行机构输出幅值是有限的,即输入饱和问题,该问题是目前控制系统中最为常见的一种非线性问题。由于控制输入饱和的存在,可能导致整个控制系统发散,进而导致整个控制系统失控。即使系统不发散,长时间高强度的振荡也会导致控制系统的结构损坏,从而导致故障。控制输入饱和问题是多年来研究的热门课题。

目前解决控制输入受限下控制器的设计问题有两种方法:一种是设计有界的控制输入,例如文献[3,4]中,采用双曲正切函数设计有界的控制律,但该方法过于保守,会造成执行器利用的效率不高;另一种是基于控制输入饱和的方法,采用 LMI 方法设计控制器的增益^[1,2],实现控制输入超出界限部分的有效补偿,该方法与有界控制输入方法相比,可保证控制输入按最大的值,有效地提高了执行器的利用效率。

近些年来国内外的学者对抗饱和问题进行了深入的研究,线性矩阵不等式 LMI 作为一种有效的数学工具,被广泛地应用于抗饱和控制领域之中。G. Grimm 等^[2]针对一般情况下的稳定模型系统设计了基于 LMI 的动态补偿器,保证系统稳定,并保证系统输出对外部干扰具有 L_2 增益。H. S. Hu 等^[5]针对一般系统研究了基于 LMI 的 L_2 增益特性及稳定区域。

本章针对控制系统抗饱和问题,介绍了基于 LMI 的抗饱和补偿器,保证了系统在输入受限情况下闭环稳定。

5.1 LQG 控制器的设计

5.1.1 系统描述

考虑如下模型

$$\begin{aligned}\dot{\mathbf{x}}_p &= \mathbf{A}_p \mathbf{x}_p + \mathbf{B}_{pu} u + \mathbf{B}_{pw} \mathbf{w} \\ y &= \mathbf{C}_{py} \mathbf{x}_p + \mathbf{D}_{pyu} u + \mathbf{D}_{pyw} \mathbf{w} + v_0\end{aligned}\quad (5.1)$$

其中, $\mathbf{x}_p = [x_1 \ x_2]^T$, $\mathbf{w} = [\omega_0 \ r]^T$, $\mathbf{B}_{pw} = [\mathbf{B}_{pw0} \ \mathbf{B}_{pwr}]$, $\mathbf{D}_{pyw} = [\mathbf{D}_{pyw0} \ \mathbf{D}_{pywr}]$, $\mathbf{B}_{pwr} = 0$, $\mathbf{D}_{pywr} = 0$, r 为指令, ω_0 和 v_0 分别为加在输入和输出的信号噪声。

5.1.2 控制器的设计

LQG 控制器由 LQI 控制器和 Kalman 滤波器组合构成,如图 5.1 所示。采用 Kalman 滤波器实现文献[1]中控制器式(4.9)的动态系统结构,同时可实现信号的滤波。

采用带有积分的 LQG 控制器结构如图 5.2 所示,其中 x_i 为跟踪误差的积分。采用 lqi()函数求控制器增益 K ,采用 Kalman 滤波器实现动态系统的状态估计。

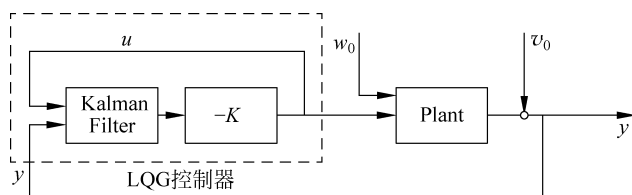


图 5.1 LQG 控制系统结构

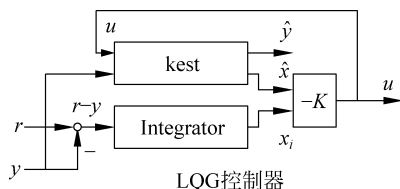


图 5.2 带有积分的 LQG 控制器结构

针对模型式(5.1),Kalman 滤波算法为

$$\dot{\hat{x}} = A_p \hat{x} + B_{pu} u + L(y - C_{py} \hat{x} - D_{pyu} u) \quad (5.2)$$

其中, L 为 kalman 增益。

采用如下命令实现 Kalman 滤波算法,从而求得增益 L :

$$[\text{kest}, L, P] = \text{kalman}(\text{sys}, Q_n, R_n, N_n) \quad (5.3)$$

其中, $\text{sys} = \text{ss}(A_p, B_{pu}, C_{py}, D_{pyu})$ 将模型式(5.1)转换为状态空间的形式,kest 为 Kalman 滤波器的结构信息, Q_n, R_n 分别表示输入噪声 w_0 和输出噪声 v_0 的协方差数据, $Q_n = E(w_0 w_0^T), R_n = E(v_0 v_0^T), P$ 为 Riccati 方程的信息。

二次型性能指标为

$$J(u) = \int_0^\infty \{ \bar{x}^T Q \bar{x} + 2 \bar{x}^T N u + u^T R u \} dt \quad (5.4)$$

其中, $\bar{x} = [\hat{x} \ x_i]^T, Q, R, N$ 分别为描述状态和控制输入的权值矩阵。

采用 MATLAB 中的 lqi()函数,可求得满足二次型性能指标的最优控制增益和控制器为

$$K = \text{lqi}(\text{sys}, Q, R, N) \quad (5.5)$$

$$u = -K \bar{x} = -K_x \hat{x} - K_i x_i \quad (5.6)$$

其中, x_i 为跟踪误差的积分, $K = [K_x \ K_i], \dot{x}_i = r - y$ 。

控制目标为: 在 $\hat{x}$ 和 u 尽量减小的情况下,保证 $x_i \rightarrow 0$,即 $r \rightarrow y$ 。

在 Kalman 滤波器中,由于

$$\begin{aligned} & \mathbf{A}_p \hat{\mathbf{x}} + \mathbf{B}_{pu} u + \mathbf{L}(y - \mathbf{C}_{py} \hat{\mathbf{x}} - \mathbf{D}_{pyu} u) \\ &= \mathbf{A}_p \hat{\mathbf{x}} - \mathbf{B}_{pu} \mathbf{K}_x \hat{\mathbf{x}} - \mathbf{B}_{pu} \mathbf{K}_i x_i + \mathbf{L}y - \mathbf{L}\mathbf{C}_{py} \hat{\mathbf{x}} + \mathbf{L}\mathbf{D}_{pyu} \mathbf{K}_x \hat{\mathbf{x}} + \mathbf{L}\mathbf{D}_{pyu} \mathbf{K}_i x_i \\ &= (\mathbf{A}_p - \mathbf{B}_{pu} \mathbf{K}_x - \mathbf{L}\mathbf{C}_{py} + \mathbf{L}\mathbf{D}_{pyu} \mathbf{K}_x) \hat{\mathbf{x}} + (-\mathbf{B}_{pu} \mathbf{K}_i + \mathbf{L}\mathbf{D}_{pyu} \mathbf{K}_i) x_i + \mathbf{L}y \end{aligned}$$

则 LQG 控制器算法状态方程可写为

$$\begin{bmatrix} \dot{\hat{\mathbf{x}}} \\ \dot{x}_i \end{bmatrix} = \begin{bmatrix} \mathbf{A}_p - \mathbf{B}_{pu} \mathbf{K}_x - \mathbf{L}\mathbf{C}_{py} + \mathbf{L}\mathbf{D}_{pyu} \mathbf{K}_x & -\mathbf{B}_{pu} \mathbf{K}_i + \mathbf{L}\mathbf{D}_{pyu} \mathbf{K}_i \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \hat{\mathbf{x}} \\ x_i \end{bmatrix} + \begin{bmatrix} 0 & \mathbf{L} \\ 1 & -1 \end{bmatrix} \begin{bmatrix} r \\ y \end{bmatrix} \quad (5.7)$$

其中, $\begin{bmatrix} 0 & \mathbf{L} \\ 1 & -1 \end{bmatrix} \begin{bmatrix} r \\ y \end{bmatrix} = \begin{bmatrix} \mathbf{L} \\ -1 \end{bmatrix} y + \begin{bmatrix} 0 \\ 1 \end{bmatrix} r$ 。

5.1.3 闭环系统的状态方程表示

根据式(5.1),可知被控对象状态方程

$$\begin{aligned} \dot{\mathbf{x}}_p &= \mathbf{A}_p \mathbf{x}_p + \mathbf{B}_{pu} u + \mathbf{B}_{pw0} w_0 \\ y &= \mathbf{C}_{py} \mathbf{x}_p + \mathbf{D}_{pyu} u + \mathbf{D}_{pyw0} w_0 + v_0 \end{aligned} \quad (5.8)$$

根据式(5.6)和式(5.7),可将 LQG 控制器算法写成状态方程形式

$$\begin{aligned} \dot{\mathbf{x}}_c &= \mathbf{A}_c \mathbf{x}_c + \mathbf{B}_{cy} y + \mathbf{B}_{cw} w \\ u &= \mathbf{C}_c \mathbf{x}_c + \mathbf{D}_{cy} y + \mathbf{D}_{cw} w \end{aligned} \quad (5.9)$$

其中, $\mathbf{x}_c = \begin{bmatrix} \hat{\mathbf{x}} \\ x_i \end{bmatrix}$, $\mathbf{A}_c = \begin{bmatrix} \mathbf{A}_p - \mathbf{B}_{pu} \mathbf{K}_x - \mathbf{L}\mathbf{C}_{py} + \mathbf{L}\mathbf{D}_{pyu} \mathbf{K}_x & -\mathbf{B}_{pu} \mathbf{K}_i + \mathbf{L}\mathbf{D}_{pyu} \mathbf{K}_i \\ 0 & 0 \end{bmatrix}$, $\mathbf{B}_{cy} = \begin{bmatrix} \mathbf{L} \\ -1 \end{bmatrix}$, $\mathbf{B}_{cw} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 1 \end{bmatrix}$, $\mathbf{C}_c = -\mathbf{K}$, $\mathbf{D}_{cy} = 0$, $\mathbf{D}_{cw} = \begin{bmatrix} 0 & 0 \end{bmatrix}$ 。

5.1.4 仿真实例

被控对象取式(5.1),即

$$\begin{aligned} \dot{x}_1 &= x_2 \\ \dot{x}_2 &= -x_1 - 10x_2 + u + w_0 \\ y &= x_1 + w_0 + v_0 \end{aligned}$$

对应式(5.1), $\mathbf{A}_p = \begin{bmatrix} 0 & 1 \\ -1 & -10 \end{bmatrix}$, $\mathbf{B}_{pu} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$, $\mathbf{B}_{pw} = \mathbf{B}_{pu}$, $\mathbf{C}_{py} = \begin{bmatrix} 1 & 0 \end{bmatrix}$, $\mathbf{D}_{pyu} = 0$, $\mathbf{D}_{pyw0} = 1$, w_0 和 v_0 分别为加在输入和输出的信号噪声, $w_0 = 0.001\sin(10t)$, $v_0 = 0.001\text{rands}(1)$ 。

通过 LQI 方法求控制增益 $\mathbf{K}$, 根据二次型性能指标式(5.4), 不考虑 w_0 和输出噪声

v_0 之间的相互影响,取 $Q = \begin{bmatrix} 5 & 0 & 0 \\ 0 & 5 & 0 \\ 0 & 0 & 60 \end{bmatrix}$, $R = 0.001$, $N = 0$, 利用 $K = \text{lqi}(\text{sys}, Q, R, N)$ 求得 $K = -C_c = [202.3428 \quad 64.1936 \quad -244.949]$ 。

通过 Kalman 滤波算法求增益 L , 根据式(5.3), 将输入噪声 w_0 和输出噪声 v_0 的协方差数据分别取为 $Q_n = 100$, $R_n = 100$, 利用 $[\text{kalmf}, L] = \text{kalmf}(\text{Plant}, Q_n, R_n)$ 求得增益 $L = \begin{bmatrix} 0.008 \\ 0.50 \end{bmatrix}$, 从而得到控制器式(5.9)。取指令 r 为方波信号, $r = 1.5\text{square}(0.25t)$, 仿真结果如图 5.3 和图 5.4 所示。

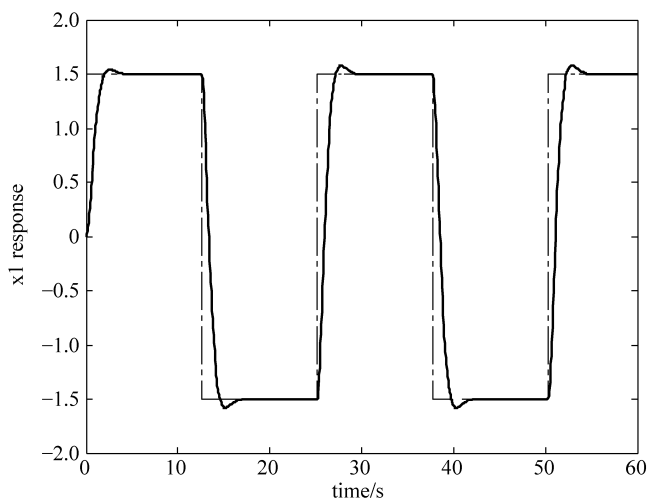


图 5.3 x_1 的方波响应

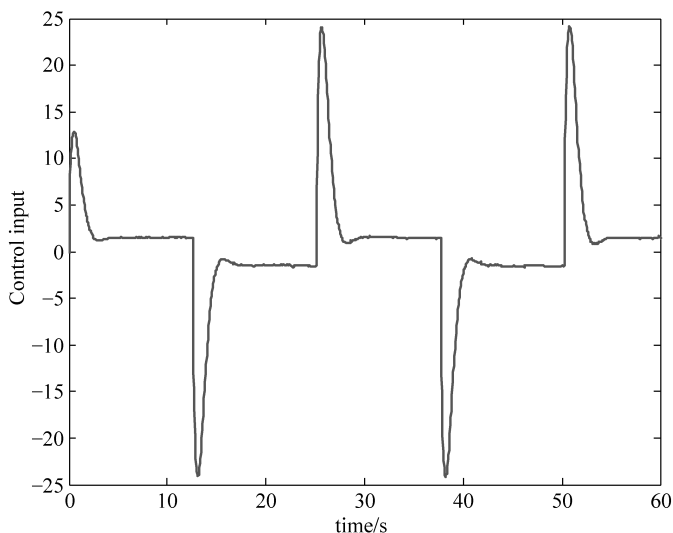


图 5.4 控制输入

仿真程序：

(1) LQG 控制器设计程序：chap5_1LQG.m

```
% LQG Controller design
clear all;
close all;

% Plant
Ap = [0 1; -1 -10];
Bpu = [0;1];
Bpw0 = Bpu;
Cpy = [1 0];
Dpyu = 0;
Dpyw0 = 1;

% LQI design
sys = ss(Ap,Bpu,Cpy,Dpyu); % in state space without noise
Q = [5 0 0;0 5 0;0 0 60]; % Used in lqi for x and xi
R = 0.001;
N = 0;
K = lqi(sys,Q,R,N);

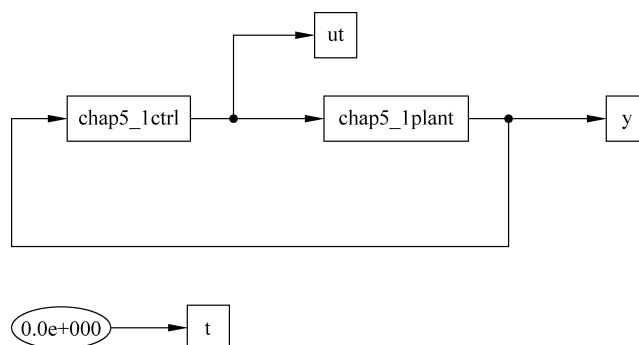
Kx = [K(1) K(2)];
Ki = K(3);
% Kalman filter
Plant = ss(Ap,[Bpu Bpw0],Cpy,[Dpyu Dpyw0]); % in state space with noise
Qn = 100;Rn = 100;
[kalmf,L] = kalman(Plant,Qn,Rn);

% LQG controller
Ac = [Ap - Bpu * Kx - L * Cpy + L * Dpyu * Kx - Bpu * Ki + L * Dpyu * Ki;
      0 0 0];
Bcy = [L; -1];
Bcw = [0 0;0 0;0 1];

Cc = -K
Dcy = 0;
Dcw = [0 0];

save lqg_file Ac Bcy Bcw Cc Dcy Dcw;
```

(2) Simulink 主程序：chap5_1sim.mdl



(3) 控制器程序: chap5_1ctrl.m

```

function [sys,x0,str,ts] = s_function(t,x,u,flag)
switch flag,
case 0,
    [sys,x0,str,ts] = mdlInitializeSizes;
case 1,
    sys = mdlDerivatives(t,x,u);
case 3,
    sys = mdlOutputs(t,x,u);
case {1,2, 4, 9 }
    sys = [];
otherwise
    error(['Unhandled flag = ',num2str(flag)]);
end
function [sys,x0,str,ts] = mdlInitializeSizes
sizes = simsizes;
sizes.NumContStates = 3;
sizes.NumDiscStates = 0;
sizes.NumOutputs = 1;
sizes.NumInputs = 1;
sizes.DirFeedthrough = 1;
sizes.NumSampleTimes = 1;
sys = simsizes(sizes);
x0 = [0 0 0];
str = [];
ts = [0 0];
function sys = mdlDerivatives(t,x,u)
r = 1.5 * square(0.25 * t);
y = u(1);

load lqq_file; % Ac,Bcy,Bcw
sys(1:3) = Ac * x + Bcy * y + Bcw(:,2) * r;
function sys = mdlOutputs(t,x,u)
r = 1.5 * square(0.25 * t);
y = u(1);
load lqq_file; % Cc,Dcy,Dcw

xc = [x(1) x(2) x(3)]';
ut = Cc * xc + Dcy * y + Dcw(:,2) * r;

sys(1) = ut;

```

(4) 被控对象程序: chap5_1plant.m

```

function [sys,x0,str,ts] = s_function(t,x,u,flag)
switch flag,
case 0,
    [sys,x0,str,ts] = mdlInitializeSizes;
case 1,
    sys = mdlDerivatives(t,x,u);

```

```

case 3,
    sys = mdlOutputs(t,x,u);
case {2, 4, 9 }
    sys = [];
otherwise
    error(['Unhandled flag = ',num2str(flag)]);
end
function [sys,x0,str,ts] = mdlInitializeSizes
    sizes = simsizes;
    sizes.NumContStates = 2;
    sizes.NumDiscStates = 0;
    sizes.NumOutputs = 1;
    sizes.NumInputs = 1;
    sizes.DirFeedthrough = 1;
    sizes.NumSampleTimes = 1;
    sys = simsizes(sizes);
    x0 = [0 0];
    str = [];
    ts = [0 0];
    function sys = mdlDerivatives(t,x,u)
        ut = u(1);
        w0 = 0.001 * sin(10 * t);
        Ap = [0 1; -1 -10];
        Bpu = [0;1];
        Bpw0 = Bpu;
        sys(1:2) = Ap * x + Bpu * ut + Bpw0 * w0;
        function sys = mdlOutputs(t,x,u)
            ut = u(1); % sizes.DirFeedthrough = 1
            Cpy = [1 0];
            Dpyu = 0;
            Dpyw0 = 1;
            w0 = 0.001 * sin(10 * t);
            v0 = 0.001 * rand(1);
            sys = Cpy * x + Dpyu * ut + Dpyw0 * w0 + v0;

```

(5) 作图程序: chap5_1plot.m

```

close all;
r = 1.5 * square(0.25 * t);

figure(1);
plot(t,r,'-r',t,y,'k','linewidth',2);
xlabel('time(s)');ylabel('x1 response');

figure(2);
plot(t,ut(:,1),'r','linewidth',2);
xlabel('time(s)');ylabel('Control input');

```

5.2 基于 LMI 的抗饱和和闭环系统描述

5.2.1 系统描述

忽略噪声影响,仍考虑模型式(5.1),即

$$\begin{aligned}\dot{\mathbf{x}}_p &= \mathbf{A}_p \mathbf{x}_p + \mathbf{B}_{pu} u + \mathbf{B}_{pw} \mathbf{w} \\ y &= \mathbf{C}_{py} \mathbf{x}_p + \mathbf{D}_{pyu} u + \mathbf{D}_{pyw} \mathbf{w}\end{aligned}\quad (5.10)$$

控制的目的是通过施加一个控制输入 u , 使 $y \rightarrow r$ 。由于输入受限部分的存在, 闭环系统可能发散或者产生激烈的振荡, 为保证系统稳定, 需要设计抗饱和补偿器, 控制输入受限控制系统如图 5.5 所示。

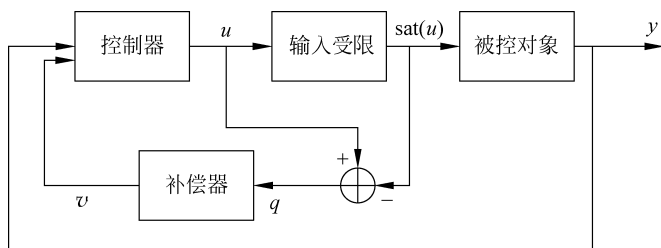


图 5.5 抗饱和和补偿控制系统

控制输入饱和函数表达如下

$$\text{sat}(u) = \begin{cases} \bar{u}, & u > \bar{u} \\ u, & -\bar{u} \leq u \leq \bar{u} \\ -\bar{u}, & u < -\bar{u} \end{cases} \quad (5.11)$$

其中, u 为理论上的控制输入, 取

$$q = u - \text{sat}(u)$$

5.2.2 闭环系统的描述

参考文献[1]的设计方法, 设计如下:

(1) 模型式(5.10)的位置状态方程表示

定义状态 $\mathbf{x}_p$, 输出为 y , 性能输出函数为 z , 则式(5.10)可写为

$$\begin{aligned}\dot{\mathbf{x}}_p &= \mathbf{A}_p \mathbf{x}_p + \mathbf{B}_{pu} u + \mathbf{B}_{pw} \mathbf{w} \\ y &= \mathbf{C}_{py} \mathbf{x}_p + \mathbf{D}_{pyu} u + \mathbf{D}_{pyw} \mathbf{w} \\ z &= \mathbf{C}_{pz} \mathbf{x}_p + \mathbf{D}_{pzu} u + \mathbf{D}_{pzw} \mathbf{w}\end{aligned}\quad (5.12)$$

(2) 设计抗饱和控制器

通过 LQG 控制器算法设计常规控制器式(5.9), 在此基础上, 设计抗饱和控制器如下:

$$\begin{aligned}\dot{\mathbf{x}}_c &= \mathbf{A}_c \mathbf{x}_c + \mathbf{B}_{cy} \mathbf{y} + \mathbf{B}_{cw} \mathbf{w} + \mathbf{v}_1 \\ u &= \mathbf{C}_c \mathbf{x}_c + \mathbf{D}_{cy} \mathbf{y} + \mathbf{D}_{cw} \mathbf{w} + \mathbf{v}_2\end{aligned}\quad (5.13)$$

其中, $\mathbf{v}_1$ 和 $\mathbf{v}_2$ 为待求的补偿项。

(3) 输入受限时, 不加补偿器 $\mathbf{v}$

此时式(5.12)可表示为

$$\begin{aligned}\dot{\mathbf{x}}_p &= \mathbf{A}_p \mathbf{x}_p + \mathbf{B}_{pu} \text{sat}(u) + \mathbf{B}_{pw} \mathbf{w} \\ \mathbf{y} &= \mathbf{C}_{py} \mathbf{x}_p + \mathbf{D}_{pyu} \text{sat}(u) + \mathbf{D}_{pyw} \mathbf{w} \\ \mathbf{z} &= \mathbf{C}_{pz} \mathbf{x}_p + \mathbf{D}_{pzu} \text{sat}(u) + \mathbf{D}_{pzw} \mathbf{w}\end{aligned}\quad (5.14)$$

式(5.13)表示为

$$\begin{aligned}\dot{\mathbf{x}}_c &= \mathbf{A}_c \mathbf{x}_c + \mathbf{B}_{cy} \mathbf{y} + \mathbf{B}_{cw} \mathbf{w} \\ u &= \mathbf{C}_c \mathbf{x}_c + \mathbf{D}_{cy} \mathbf{y} + \mathbf{D}_{cw} \mathbf{w}\end{aligned}\quad (5.15)$$

由 $q = u - \text{sat}(u)$, 式(5.14)可写为

$$\begin{aligned}\dot{\mathbf{x}}_p &= \mathbf{A}_p \mathbf{x}_p + \mathbf{B}_{pu} (u - q) + \mathbf{B}_{pw} \mathbf{w} \\ \mathbf{y} &= \mathbf{C}_{py} \mathbf{x}_p + \mathbf{D}_{pyu} (u - q) + \mathbf{D}_{pyw} \mathbf{w} \\ \mathbf{z} &= \mathbf{C}_{pz} \mathbf{x}_p + \mathbf{D}_{pzu} (u - q) + \mathbf{D}_{pzw} \mathbf{w}\end{aligned}\quad (5.16)$$

将式(5.16)中的 $\mathbf{y}$ 代入式(5.15), 可得

$$u = \mathbf{C}_c \mathbf{x}_c + \mathbf{D}_{cy} [\mathbf{C}_{py} \mathbf{x}_p + \mathbf{D}_{pyu} (u - q) + \mathbf{D}_{pyw} \mathbf{w}] + \mathbf{D}_{cw} \mathbf{w}$$

即

$$u = \mathbf{C}_c \mathbf{x}_c + \mathbf{D}_{cy} \mathbf{C}_{py} \mathbf{x}_p + \mathbf{D}_{cy} \mathbf{D}_{pyu} (u - q) + \mathbf{D}_{cy} \mathbf{D}_{pyw} \mathbf{w} + \mathbf{D}_{cw} \mathbf{w}$$

从而

$$u = (1 - \mathbf{D}_{cy} \mathbf{D}_{pyu})^{-1} [\mathbf{C}_c \mathbf{x}_c + \mathbf{D}_{cy} \mathbf{C}_{py} \mathbf{x}_p - \mathbf{D}_{cy} \mathbf{D}_{pyu} q + (\mathbf{D}_{cy} \mathbf{D}_{pyw} + \mathbf{D}_{cw}) \mathbf{w}]$$

定义 $\mathbf{x}_{cl} = [\mathbf{x}_p \quad \mathbf{x}_c]^T$, $\Delta u = (1 - \mathbf{D}_{cy} \mathbf{D}_{pyu})^{-1}$, 则 $\Delta u (1 - \mathbf{D}_{cy} \mathbf{D}_{pyu}) = \mathbf{I}$, 及

$$\mathbf{I} - \Delta u = -\Delta u \mathbf{D}_{cy} \mathbf{D}_{pyu}$$

从而可得

$$u = \Delta u [\mathbf{D}_{cy} \mathbf{C}_{py} \quad \mathbf{C}_c] \mathbf{x}_{cl} + (\mathbf{I} - \Delta u) q + \Delta u (\mathbf{D}_{cy} \mathbf{D}_{pyw} + \mathbf{D}_{cw}) \mathbf{w} \quad (5.17)$$

将式(5.17)代入式(5.16)中的 $\dot{\mathbf{x}}_p$, 可得

$$\begin{aligned}\dot{\mathbf{x}}_p &= \mathbf{A}_p \mathbf{x}_p + \mathbf{B}_{pu} [\Delta u [\mathbf{D}_{cy} \mathbf{C}_{py} \quad \mathbf{C}_c] \mathbf{x}_{cl} - \Delta u q + \Delta u (\mathbf{D}_{cy} \mathbf{D}_{pyw} + \mathbf{D}_{cw}) \mathbf{w}] + \mathbf{B}_{pw} \mathbf{w} \\ &= [\mathbf{A}_p + \mathbf{B}_{pu} \Delta u \mathbf{D}_{cy} \mathbf{C}_{py} \quad \mathbf{B}_{pu} \Delta u \mathbf{C}_c] \mathbf{x}_{cl} + \mathbf{B}_{pu} [-\Delta u q + \Delta u (\mathbf{D}_{cy} \mathbf{D}_{pyw} + \mathbf{D}_{cw}) \mathbf{w}] + \mathbf{B}_{pw} \mathbf{w}\end{aligned}\quad (5.18)$$

将式(5.17)代入式(5.16)中的 $\mathbf{y}$, 可得

$$\mathbf{y} = \mathbf{C}_{py} \mathbf{x}_p + \mathbf{D}_{pyu} \{\Delta u [\mathbf{D}_{cy} \mathbf{C}_{py} \quad \mathbf{C}_c] \mathbf{x}_{cl} - \Delta u q + \Delta u (\mathbf{D}_{cy} \mathbf{D}_{pyw} + \mathbf{D}_{cw}) \mathbf{w}\} + \mathbf{D}_{pyw} \mathbf{w} \quad (5.19)$$

将式(5.19)代入式(5.15)中的 $\dot{\mathbf{x}}_c$, 可得

$$\begin{aligned}\dot{\mathbf{x}}_c &= \mathbf{A}_c \mathbf{x}_c + \mathbf{B}_{cy} \{\mathbf{C}_{py} \mathbf{x}_p + \mathbf{D}_{pyu} [\Delta u [\mathbf{D}_{cy} \mathbf{C}_{py} \quad \mathbf{C}_c] \mathbf{x}_{cl} - \Delta u q + \Delta u (\mathbf{D}_{cy} \mathbf{D}_{pyw} + \mathbf{D}_{cw}) \mathbf{w}] + \\ &\quad \mathbf{D}_{pyw} \mathbf{w}\} + \mathbf{B}_{cw} \mathbf{w} \\ &= [\mathbf{B}_{cy} \mathbf{D}_{pyu} \Delta u \mathbf{D}_{cy} \mathbf{C}_{py} + \mathbf{B}_{cy} \mathbf{C}_{py} \quad \mathbf{A}_c + \mathbf{B}_{cy} \mathbf{D}_{pyu} \Delta u \mathbf{C}_c] \mathbf{x}_{cl} - \mathbf{B}_{cy} \mathbf{D}_{pyu} \Delta u q +\end{aligned}$$

$$[B_{cy}D_{pyu}\Delta u(D_{cy}D_{pyw}+D_{cw})+B_{cy}D_{pyw}+B_{cw}]w \quad (5.20)$$

由于 $(1-D_{pyu}D_{cy})D_{pyu}=D_{pyu}(1-D_{cy}D_{pyu})$,则

$$D_{pyu}(I-D_{cy}D_{pyu})^{-1}=(I-D_{pyu}D_{cy})^{-1}D_{pyu}$$

定义 $\Delta y=(I-D_{pyu}D_{cy})^{-1}$,又由于 $\Delta u=(I-D_{cy}D_{pyu})^{-1}$,则

$$\Delta y D_{pyu} D_{cy} + I = \Delta y \text{ 且 } D_{pyu} \Delta u = \Delta y D_{pyu}$$

则式(5.20)中的各项可整理为

$$\begin{aligned} & B_{cy}B_{pyu}\Delta u B_{cy}C_{py} + B_{cy}C_{py} = B_{cy}(B_{pyu}\Delta u B_{cy} + I)C_{py} \\ & = B_{cy}(\Delta y D_{pyu} B_{cy} + I)C_{py} = B_{cy}\Delta y C_{py} - B_{cy}D_{pyu}\Delta u = -B_{cy}\Delta y D_{pyu} \\ & B_{cy}B_{pyu}\Delta u(D_{cy}D_{pyw}+D_{cw}) + B_{cy}B_{pyw} + B_{cw} \\ & = B_{cy}\Delta y D_{pyu}(D_{cy}D_{pyw}+D_{cw}) + B_{cy}B_{pyw} + B_{cw} \\ & = B_{cy}\Delta y D_{pyu}D_{cy}D_{pyw} + B_{cy}B_{pyw} + B_{cy}\Delta y D_{pyu}D_{cw} + B_{cw} \\ & = B_{cy}\Delta y(B_{pyw}+D_{pyu}D_{cw}) + B_{cw} \end{aligned}$$

其中, $B_{cy}\Delta y D_{pyu}D_{cy}D_{pyw}+B_{cy}B_{pyw}=B_{cy}(\Delta y D_{pyu}D_{cy}+I)D_{pyw}=B_{cy}\Delta y B_{pyw}$ 。

则

$$\dot{x}_c = [B_{cy}\Delta y C_{py}A_c + B_{cy}\Delta y D_{pyu}C_c]x_{cl} - B_{cy}\Delta y D_{pyu}q + [B_{cy}\Delta y(D_{pyw}+D_{pyu}D_{cw})+B_{cw}]w \quad (5.21)$$

将式(5.17)代入式(5.16),并根据 $I-\Delta u=-\Delta u D_{cy}D_{pyu}$ 和式(5.19),可得

$$\begin{aligned} z &= C_{pz}x_p + D_{pzu}[\Delta u[D_{cy}C_{py} \quad C_c]x_{cl} - \Delta u D_{cy}D_{pyu}q + \Delta u(D_{cy}D_{pyw}+D_{cw})w - q] + D_{pzw}w \\ &= [C_{pz} + D_{pzu}\Delta u D_{cy}C_{py} \quad D_{pzu}\Delta u C_c]x_{cl} - D_{pzu}(\Delta u D_{cy}D_{pyu} + I)q + \\ &= [D_{pzu}\Delta u(D_{cy}D_{pyw}+D_{cw}) + D_{pzw}]w \\ &= [C_{pz} + D_{pzu}\Delta u D_{cy}C_{py} \quad D_{pzu}\Delta u C_c]x_{cl} - D_{pzu}\Delta u q + \\ & \quad [D_{pzu}\Delta u(D_{cy}D_{pyw}+D_{cw}) + D_{pzw}]w \end{aligned} \quad (5.22)$$

由式(5.17)、(5.18)、(5.21)和式(5.22)可得闭环系统的表示形式如下:

$$\begin{aligned} u &= \Delta u[D_{cy}C_{py} \quad C_c]x_{cl} + (I - \Delta u)q + \Delta u(D_{cy}D_{pyw} + D_{cw})w \\ \dot{x}_p &= [A_p + B_{pu}\Delta u D_{cy}C_{py} \quad B_{pu}\Delta u C_c]x_{cl} + B_{pu}[-\Delta u q + \Delta u(D_{cy}D_{pyw} + D_{cw})w] + B_{pw}w \\ \dot{x}_c &= [B_{cy}\Delta y C_{py} \quad A_c + B_{cy}\Delta y D_{pyu}C_c]x_{cl} - B_{cy}\Delta y D_{pyu}q + [B_{cy}\Delta y(D_{pyw} + D_{pyu}D_{cw}) + B_{cw}]w \\ z &= [C_{pz} + D_{pzu}\Delta u D_{cy}C_{py} \quad D_{pzu}\Delta u C_c]x_{cl} - D_{pzu}\Delta u q + [D_{pzu}\Delta u(D_{cy}D_{pyw} + D_{cw}) + D_{pzw}]w \end{aligned}$$

从而可得闭环系统为

$$\begin{aligned} \dot{x}_{cl} &= A_{cl}x_{cl} + B_{clq}q + B_{clw}w \\ z &= C_{clz}x_{cl} + D_{clzq}q + D_{clzw}w \\ u &= C_{clu}x_{cl} + D_{cluq}q + D_{cluw}w \end{aligned} \quad (5.23)$$

式(5.23)中采用了如下定义:

$$A_{cl} = \begin{bmatrix} A_p + B_{pu}\Delta u D_{cy}C_{py} & B_{pu}\Delta u C_c \\ B_{cy}\Delta y C_{py} & A_c + B_{cy}\Delta y D_{pyu}C_c \end{bmatrix}, \quad B_{clq} = \begin{bmatrix} -B_{pu}\Delta u \\ -B_{cy}\Delta y D_{pyu} \end{bmatrix},$$

$$\begin{aligned} \mathbf{B}_{clw} &= \begin{bmatrix} \mathbf{B}_{pw} + \mathbf{B}_{pu} \Delta u (\mathbf{D}_{cy} \mathbf{D}_{pyw} + \mathbf{D}_{cw}) \\ \mathbf{B}_{cw} + \mathbf{B}_{cy} \Delta y (\mathbf{D}_{pyw} + \mathbf{D}_{pyu} \mathbf{D}_{cw}) \end{bmatrix}, \quad \mathbf{C}_{clz} = [\mathbf{C}_{pz} + \mathbf{D}_{pzu} \Delta u \mathbf{D}_{cy} \mathbf{C}_{py} \quad \mathbf{D}_{pzu} \Delta u \mathbf{C}_c], \\ \mathbf{D}_{clzq} &= -\mathbf{D}_{pzu} \Delta u, \quad \mathbf{D}_{clzw} = \mathbf{D}_{pzu} \Delta u (\mathbf{D}_{cy} \mathbf{D}_{pyw} + \mathbf{D}_{cw}) + \mathbf{D}_{pzw}, \quad \mathbf{C}_{clu} = \Delta u [\mathbf{D}_{cy} \mathbf{C}_{py} \quad \mathbf{C}_c], \\ \Delta \mathbf{D}_{cluq} &= \mathbf{I} - \Delta u, \quad \mathbf{D}_{cluw} = \Delta u (\mathbf{D}_{cy} \mathbf{D}_{pyw} + \mathbf{D}_{cw}), \quad \Delta y = (\mathbf{I} - \mathbf{D}_{pyu} \mathbf{D}_{cy})^{-1}, \\ \Delta u &= (\mathbf{I} - \mathbf{D}_{cy} \mathbf{D}_{pyu})^{-1}. \end{aligned}$$

(4) 输入受限时,加补偿器

此时式(5.10)可表示为

$$\begin{aligned} \dot{\mathbf{x}}_p &= \mathbf{A}_p \mathbf{x}_p + \mathbf{B}_{pu} u + \mathbf{B}_{pw} \mathbf{w} \\ y &= \mathbf{C}_{py} \mathbf{x}_p + \mathbf{D}_{pyu} u + \mathbf{D}_{pyw} \mathbf{w} \\ z &= \mathbf{C}_{pz} \mathbf{x}_p + \mathbf{D}_{pzu} u + \mathbf{D}_{pzw} \mathbf{w} \end{aligned} \quad (5.24)$$

式(5.15)表示为

$$\begin{aligned} \dot{\mathbf{x}}_c &= \mathbf{A}_c \mathbf{x}_c + \mathbf{B}_{cy} y + \mathbf{B}_{cw} \mathbf{w} + v_1 \\ u &= \mathbf{C}_c \mathbf{x}_c + \mathbf{D}_{cy} y + \mathbf{D}_{cw} \mathbf{w} + v_2 \end{aligned} \quad (5.25)$$

由 $q = u - \text{sat}(u)$, 式(5.13)可写为

$$\begin{aligned} \dot{\mathbf{x}}_p &= \mathbf{A}_p \mathbf{x}_p + \mathbf{B}_{pu} (u - q) + \mathbf{B}_{pw} \mathbf{w} \\ y &= \mathbf{C}_{py} \mathbf{x}_p + \mathbf{D}_{pyu} (u - q) + \mathbf{D}_{pyw} \mathbf{w} \\ z &= \mathbf{C}_{pz} \mathbf{x}_p + \mathbf{D}_{pzu} (u - q) + \mathbf{D}_{pzw} \mathbf{w} \end{aligned} \quad (5.26)$$

将式(5.26)中的 $y = \mathbf{C}_{py} \mathbf{x}_p + \mathbf{D}_{pyu} (u - q) + \mathbf{D}_{pyw} \mathbf{w}$ 代入式(15), 可得

$$u = \mathbf{C}_c \mathbf{x}_c + \mathbf{D}_{cy} (\mathbf{C}_{py} \mathbf{x}_p + \mathbf{D}_{pyu} (u - q) + \mathbf{D}_{pyw} \mathbf{w}) + \mathbf{D}_{cw} \mathbf{w} + [0 \quad \mathbf{I}] \mathbf{D}_{aw} q$$

即

$$u = \mathbf{C}_c \mathbf{x}_c + \mathbf{D}_{cy} \mathbf{C}_{py} \mathbf{x}_p + \mathbf{D}_{cy} \mathbf{D}_{pyu} u - \mathbf{D}_{cy} \mathbf{D}_{pyu} q + \mathbf{D}_{cy} \mathbf{D}_{pyw} \mathbf{w} + \mathbf{D}_{cw} \mathbf{w} + [0 \quad \mathbf{I}] \mathbf{D}_{aw} q$$

由 $\Delta u = (\mathbf{I} - \mathbf{D}_{cy} \mathbf{D}_{pyu})^{-1}$ 可知 $-\Delta u \mathbf{D}_{cy} \mathbf{D}_{pyu} = \mathbf{I} - \Delta u$, 从而

$$\begin{aligned} u &= (\mathbf{I} - \mathbf{D}_{cy} \mathbf{D}_{pyu})^{-1} \{ \mathbf{C}_c \mathbf{x}_c + \mathbf{D}_{cy} \mathbf{C}_{py} \mathbf{x}_p - \mathbf{D}_{cy} \mathbf{D}_{pyu} q + \mathbf{D}_{cy} \mathbf{D}_{pyw} \mathbf{w} + \mathbf{D}_{cw} \mathbf{w} + [0 \quad \mathbf{I}] \mathbf{D}_{aw} q \} \\ &= [\Delta u \mathbf{D}_{cy} \mathbf{C}_{py} \quad \Delta u \mathbf{C}_c] \mathbf{x}_{cl} + ([0 \quad \Delta u] \mathbf{D}_{aw} - \Delta u \mathbf{D}_{cy} \mathbf{D}_{pyu}) q + \Delta u (\mathbf{D}_{cy} \mathbf{D}_{pyw} + \mathbf{D}_{cw}) \mathbf{w} \\ &= \mathbf{C}_{clu} \mathbf{x}_{cl} + (\mathbf{D}_{cluq} + \mathbf{D}_{cluv} \mathbf{D}_{aw}) q + \mathbf{D}_{cluw} \mathbf{w} \end{aligned} \quad (5.27)$$

其中, $\mathbf{D}_{cluq} = -\Delta u \mathbf{D}_{cy} \mathbf{D}_{pyu}$, $\mathbf{D}_{cluw} = -\Delta u \mathbf{D}_{cy} \mathbf{D}_{pyw} = \mathbf{I} - \Delta u$, $\mathbf{D}_{cluv} = [0 \quad \Delta u]$ 。

将式(5.27)代入式(5.26)中的 $\dot{\mathbf{x}}_p$, 可得

$$\begin{aligned} \dot{\mathbf{x}}_p &= \mathbf{A}_p \mathbf{x}_p + \mathbf{B}_{pu} (\mathbf{C}_{clu} \mathbf{x}_{cl} + (\mathbf{D}_{cluq} + \mathbf{D}_{cluv} \mathbf{D}_{aw}) q + \mathbf{D}_{cluw} \mathbf{w} - q) + \mathbf{B}_{pw} \mathbf{w} \\ &= \mathbf{A}_p \mathbf{x}_p - \mathbf{B}_{pu} q + \mathbf{B}_{pu} \{ [\Delta u \mathbf{D}_{cy} \mathbf{C}_{py} \quad \Delta u \mathbf{C}_c] \mathbf{x}_{cl} + (\mathbf{D}_{cluq} + \mathbf{D}_{cluv} \mathbf{D}_{aw}) q + \mathbf{D}_{cluw} \mathbf{w} \} + \mathbf{B}_{pw} \mathbf{w} \\ &= [\mathbf{A}_p + \mathbf{B}_{pu} \Delta u \mathbf{D}_{cy} \mathbf{C}_{py} \quad \mathbf{B}_{pu} \Delta u \mathbf{C}_c] \mathbf{x}_{cl} + (-\mathbf{B}_{pu} \Delta u + \mathbf{B}_{pu} \mathbf{D}_{cluv} \mathbf{D}_{aw}) q + \\ &\quad [\mathbf{B}_{pu} \Delta u (\mathbf{D}_{cy} \mathbf{D}_{pyw} + \mathbf{D}_{cw}) + \mathbf{B}_{pw}] \mathbf{w} \end{aligned} \quad (5.28)$$

其中, $-\mathbf{B}_{pu} q + \mathbf{B}_{pu} \mathbf{D}_{cluq} q = (-\mathbf{B}_{pu} + \mathbf{B}_{pu} \mathbf{D}_{cluq}) q = [-\mathbf{B}_{pu} + \mathbf{B}_{pu} (\mathbf{I} - \Delta u)] q = -\mathbf{B}_{pu} \Delta u q$ 。

将 u 代入 y

$$y = \mathbf{C}_{py} \mathbf{x}_p + (\mathbf{D}_{pyu} \mathbf{C}_c \mathbf{x}_c + \mathbf{D}_{pyu} \mathbf{D}_{cy} y + \mathbf{D}_{pyu} \mathbf{D}_{cw} \mathbf{w} + \mathbf{D}_{pyu} v_2 - \mathbf{D}_{pyu} q) + \mathbf{D}_{pyw} \mathbf{w}$$

则

$$\begin{aligned}
 y &= (I - D_{pyu} D_{cy})^{-1} (C_{py} x_p + D_{pyu} C_c x_c + D_{pyu} D_{cw} w + D_{pyu} v_2 - D_{pyu} q + D_{pyw} w) \\
 &= \Delta y (C_{py} x_p + D_{pyu} C_c x_c + D_{pyu} D_{cw} w + D_{pyu} v_2 - D_{pyu} q + D_{pyw} w) \\
 \dot{x}_c &= A_c x_c + B_{cy} y + B_{cw} w + v_1 \\
 &= A_c x_c + B_{cy} \Delta y (C_{py} x_p + D_{pyu} C_c x_c + D_{pyu} D_{cw} w + D_{pyu} v_2 - D_{pyu} q + D_{pyw} w) + B_{cw} w + v_1 \\
 &= A_c x_c + B_{cy} \Delta y C_{py} x_p + B_{cy} \Delta y D_{pyu} C_c x_c + B_{cy} \Delta y D_{pyu} D_{cw} w + B_{cy} \Delta y D_{pyu} v_2 - \\
 &\quad B_{cy} \Delta y D_{pyu} q + B_{cy} \Delta y D_{pyw} w + B_{cw} w + v_1 \\
 &= [B_{cy} \Delta y C_{py} \quad A_c + B_{cy} \Delta y D_{pyu} C_c] x_{cl} - B_{cy} \Delta y D_{pyu} q + (v_1 + B_{cy} \Delta y D_{pyu} v_2) + \\
 &\quad B_{cy} \Delta y (D_{pyw} + D_{pyu} D_{cw}) w + B_{cw} w \\
 &= [B_{cy} \Delta y C_{py} \quad A_c + B_{cy} \Delta y D_{pyu} C_c] x_{cl} + \{-B_{cy} \Delta y D_{pyu} + [I \quad B_{cy} \Delta y D_{pyu}] D_{aw}\} q + \\
 &\quad B_{cy} \Delta y (D_{pyw} + D_{pyu} D_{cw}) w + B_{cw} w
 \end{aligned}$$

其中, $v_1 + B_{cy} \Delta y D_{pyu} v_2 = [I \quad B_{cy} \Delta y D_{pyu}] v = [I \quad B_{cy} \Delta y D_{pyu}] D_{aw} q$ 。

将 $\dot{x}_p$ 与 $\dot{x}_c$ 合并, 可得

$$\begin{aligned}
 \begin{bmatrix} \dot{x}_p \\ \dot{x}_c \end{bmatrix} &= \begin{bmatrix} A_p + B_{pu} \Delta u D_{cy} C_{py} & B_{pu} \Delta u C_c \\ B_{cy} \Delta y C_{py} & A_c + B_{cy} \Delta y D_{pyu} C_c \end{bmatrix} \begin{bmatrix} x_p \\ x_c \end{bmatrix} + \\
 &\quad \begin{bmatrix} -B_{pu} \Delta u \\ -B_{cy} \Delta y D_{pyu} \end{bmatrix} q + \begin{bmatrix} 0 & B_{pu} D_{cluv} \\ I & B_{cy} \Delta y D_{pyu} \end{bmatrix} D_{aw} q + \\
 &\quad \begin{bmatrix} B_{pu} \Delta u (D_{cy} D_{pyw} + D_{cw}) + B_{pw} \\ B_{cy} \Delta y (D_{pyw} + D_{pyu} D_{cw}) + B_{cw} \end{bmatrix} w \\
 &= A_{cl} x_{cl} + B_{clq} q + B_{clv} D_{aw} q + B_{clw} w
 \end{aligned}$$

其中,

$$\begin{aligned}
 \begin{bmatrix} -B_{pu} \Delta u + B_{pu} D_{cluv} D_{aw} \\ -B_{cy} \Delta y D_{pyu} + [I \quad B_{cy} \Delta y D_{pyu}] D_{aw} \end{bmatrix} q &= \begin{bmatrix} -B_{pu} \Delta u \\ -B_{cy} \Delta y D_{pyu} \end{bmatrix} q + \begin{bmatrix} B_{pu} D_{cluv} \\ [I \quad B_{cy} \Delta y D_{pyu}] \end{bmatrix} D_{aw} q \\
 &= \begin{bmatrix} -B_{pu} \Delta u \\ -B_{cy} \Delta y D_{pyu} \end{bmatrix} q + \begin{bmatrix} 0 & B_{pu} \Delta u \\ I & B_{cy} \Delta y D_{pyu} \end{bmatrix} D_{aw} q \\
 &= B_{clq} q + B_{clv} D_{aw} q
 \end{aligned}$$

即

$$\dot{x}_{cl} = A_{cl} x_{cl} + (B_{clq} + B_{clv} D_{aw}) q + B_{clw} w$$

$$\begin{aligned}
 \text{其中, } B_{clq} &= \begin{bmatrix} -B_{pu} \Delta u \\ -B_{cy} \Delta y D_{pyu} \end{bmatrix}, \quad B_{clv} = \begin{bmatrix} B_{pu} D_{cluv} \\ B_{cy} D_{pyu} D_{cluv} + [I \quad 0] \end{bmatrix} = \begin{bmatrix} 0 & B_{pu} \Delta u \\ I & B_{cy} \Delta y D_{pyu} \end{bmatrix}, \\
 B_{pu} D_{cluv} &= B_{pu} [0 \quad \Delta u] = [0 \quad B_{pu} \Delta u], \quad B_{cy} D_{pyu} D_{cluv} + [I \quad 0] = B_{cy} D_{pyu} [0 \quad \Delta u] + \\
 [I \quad 0] &= [I \quad B_{cy} D_{pyu} \Delta u] = [I \quad B_{cy} \Delta y D_{pyu}].
 \end{aligned}$$

将 u 代入 z 中, 并代入 C_{clu} 、 D_{cluq} 、 D_{cluw} , 可得

$$\begin{aligned}
 z &= C_{pz} x_p + D_{pzu} u - D_{pzu} q + D_{pzw} w \\
 &= C_{pz} x_p + D_{pzu} [C_{clu} x_{cl} + (D_{cluq} + D_{cluv} D_{aw}) q + D_{cluw} w] - D_{pzu} q + D_{pzw} w \\
 &= C_{pz} x_p + D_{pzu} \{ [\Delta u D_{cy} C_{py} \quad \Delta u C_c] x_{cl} + \{ [I - \Delta u] + D_{cluv} D_{aw} \} q + \Delta u (D_{cy} D_{pyw} + \\
 &\quad D_{cw}) w \} - D_{pzu} q + D_{pzw} w \\
 &= [C_{pz} + D_{pzu} \Delta u D_{cy} C_{py} \quad D_{pzu} \Delta u C_c] x_{cl} + (-D_{pzu} \Delta u + D_{pzu} D_{cluv} D_{aw}) q + \\
 &\quad [D_{pzu} \Delta u (D_{cy} D_{pyw} + D_{cw}) + D_{pzw}] w \\
 &= [C_{pz} + D_{pzu} \Delta u D_{cy} C_{py} \quad D_{pzu} \Delta u C_c] x_{cl} + \{-D_{pzu} \Delta u + [0 \quad D_{pzu} \Delta u] D_{aw}\} q + \\
 &\quad [D_{pzu} \Delta u (D_{cy} D_{pyw} + D_{cw}) + D_{pzw}] w \\
 &= C_{clz} x_{cl} + (D_{clzq} + D_{clzv} D_{aw}) q + D_{clzw} w
 \end{aligned}$$

其中 $D_{pzu} D_{cluv} D_{aw} = D_{pzu} [0 \quad \Delta u] D_{aw} = [0 \quad D_{pzu} \Delta u] D_{aw}$ 。

$$D_{clzv} = D_{pzu} D_{cluv} = D_{pzu} [0 \quad \Delta u] = [0 \quad D_{pzu} \Delta u]$$

从而可得闭环系统

$$\begin{aligned}
 \dot{x}_{cl} &= A_{cl} x_{cl} + (B_{clv} D_{aw} + B_{clq}) q + B_{clw} w \\
 z &= C_{clz} x_{cl} + (D_{clzq} + D_{clzv} D_{aw}) q + D_{clzw} w \\
 u &= C_{clu} x_{cl} + (D_{cluq} + D_{cluv} D_{aw}) q + D_{cluw} w
 \end{aligned} \tag{5.29}$$

其中, $B_{clv} = \begin{bmatrix} 0 & B_{pu} \Delta u \\ I & B_{cy} \Delta y D_{pyu} \end{bmatrix}$, $D_{cluv} = [0 \quad \Delta u]$ 。

(5) 控制器设计

考虑被控对象模型为

$$\frac{1}{s^2 + 10s + 1}$$

上式写为状态方程形式

$$\begin{aligned}
 \dot{x}_1 &= x_2 \\
 \dot{x}_2 &= -10x_2 - x_1 + u(t) \\
 y &= x_1 \\
 z &= y - r
 \end{aligned}$$

对应于模型式(5.12)的信息为

$$A_p = \begin{bmatrix} 0 & 1 \\ -1 & -10 \end{bmatrix}, \quad B_{pu} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, \quad B_{pw} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}, \quad C_{py} = [1 \quad 0],$$

$$D_{pyu} = 0, \quad D_{pyw} = 0, \quad C_{pz} = C_{py}, \quad D_{pzu} = D_{pyu}, \quad D_{pzw} = [0 \quad -1]。$$

采用 LQG 最优控制, 可得对应于控制器(5.13)的信息为

$$A_c = \begin{bmatrix} -0.0081 & 1 & 0 \\ -203.8428 & -74.1936 & 244.9490 \\ 0 & 0 & 0 \end{bmatrix}, \quad B_{cy} = [0.0081 \quad 0.50 \quad -1.0]^T,$$

$$B_{cw} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 1 \end{bmatrix}, \quad C_c = [-202.3428 \quad -64.1936 \quad 244.9490], \quad D_{cy} = 0, D_{cw} = [0 \quad 0]。$$

控制器(5.13)中的 v_1 和 v_2 由下面补偿算法求得。

5.2.3 补偿算法设计步骤

补偿项 D_{aw} 的求法分以下几步^[1,2]：

第一步：求解最小 γ 和 R

开环系统：

$$\begin{bmatrix} R_{11}A_p^T + A_pR_{11} & B_{pw} & R_{11}C_{pz}^T \\ B_{pw}^T & -\gamma I_{nw} & D_{pzw}^T \\ C_{pz}R_{11} & D_{pzw} & -\gamma I_{nz} \end{bmatrix} < 0 \quad (5.30)$$

闭环系统：

$$\begin{bmatrix} RA_{cl}^T + A_{cl}R & B_{clw} & RC_{clz}^T \\ B_{clw}^T & -\gamma I_{nw} & D_{clzw}^T \\ C_{clz}R & D_{clzw} & -\gamma I_{nz} \end{bmatrix} < 0 \quad (5.31)$$

$$R = R^T > 0 \quad (5.32)$$

上面条件下,求使满足 $\min_{R, \gamma} \gamma$ 的 γ 和 R 。

第二步：求解 D_{aw}

基于抗饱和增益求解的 LMI 式为

$$\Psi(U, \gamma) + G_U^T \Delta_U^T H^T + H \Delta_U G_U < 0 \quad (5.33)$$

其中,

$$\Psi(U, \gamma) = \text{He} \begin{bmatrix} A_{cl}R & B_{clq}U + QC_{clu}^T & B_{clw} & QC_{clz}^T \\ 0 & D_{cluq}U - U & D_{clyw} & UD_{clzq}^T \\ 0 & 0 & -\frac{\gamma}{2}I & D_{clzw}^T \\ 0 & 0 & 0 & -\frac{\gamma}{2}I \end{bmatrix}$$

$$H = [B_{clv}^T \quad 0 \quad D_{cluv}^T \quad 0 \quad D_{clzv}^T]$$

$$G_U = [0 \quad 0 \quad I \quad 0 \quad 0]$$

其中, $\text{He}(X) = X + X^T$ 。

由于采用的是静态补偿器,故 $n_{aw}=0, Q=R$ 。

为了保证闭环系统的强稳定性, Δ_U 和 U 需要满足如下 LMI 不等式[1]:

$$-2(1-\mu)U + \text{He}(D_{cluq}U + [0_{nu \times nc} \quad I_{nu}] \Delta_U) < 0 \quad (5.34)$$

其中, μ 是很小的正实数。

求解不等式(5.30)至式(5.34),可得 Δ_U 和 U ,从而可得静态补偿器为

$$D_{aw} = \Delta_U U^{-1}, \quad v = D_{aw}q \quad (5.35)$$

5.2.4 闭环系统稳定性分析

首先,进行闭环系统稳定性分析,设计 Lyapunov 函数 $V = \mathbf{x}^T \mathbf{P} \mathbf{x}$,通过取 $\dot{V} < 0$ 并进行变换,可得到式(5.33)。

然后,根据文献[2]中的引理 5 可知,式(5.33)有解的条件是当且仅当文献[2]中式(31)成立,依据是矩阵消除定理和[2]中定理 2、定理 5 的证明,从而可得到式(5.30)至式(5.32)。

式(5.30)至式(5.33)的证明和分析来源于文献[2]。

5.2.5 仿真实例

考虑被控对象为式(5.10),初始状态为 $[0 \ 0 \ 0]$,指令为方波信号,采用 MATLAB 函数实现,取指令为 $r = 1.5\text{square}(0.08t)$ 。求解不等式式(5.30)至式(5.34),取 $v_0 = 0$,可得

$$\gamma = 2.7518, \quad \mathbf{D}_{aw} = [-0.0002 \quad 0.0019 \quad 0.0006 \quad 1.0]$$

按式(5.25)设计控制律,控制输入受限值为 $\bar{u} = 5.0$,如果加补偿器,根据式(5.35)求补偿 $v = \mathbf{D}_{aw} q$,仿真结果如图 5.6 和图 5.7 所示。如果不加补偿器,取 $\mathbf{D}_{aw} = 0, v = 0$,仿真结果如图 5.8 和图 5.9 所示。可见,加入补偿器后,方波跟踪性能和控制输入信号得到了很大的改善。

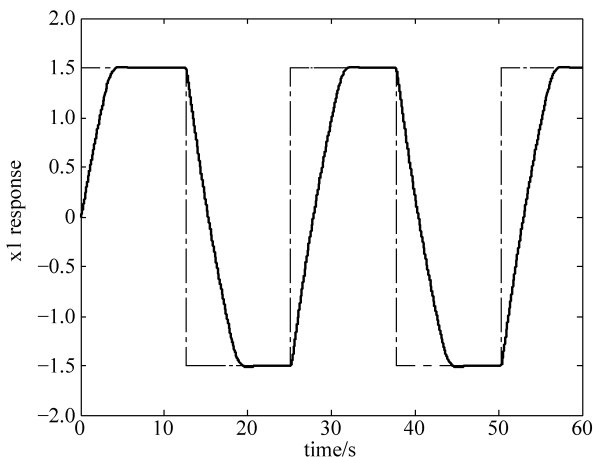


图 5.6 方波响应(加补偿器)

仿真程序:

(1) LMI 设计程序: chap5_2LMI.m

```
% Generic antiwindup LMI program
clear all;
close all;
% Dimension definition
np = 2;
```

% 被控对象动态阶数

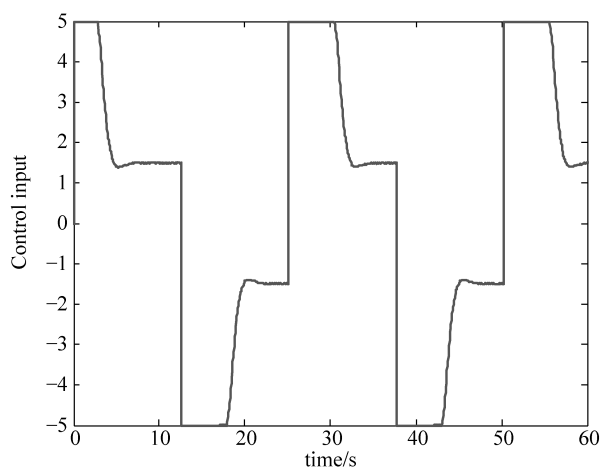


图 5.7 控制输入(加补偿器)

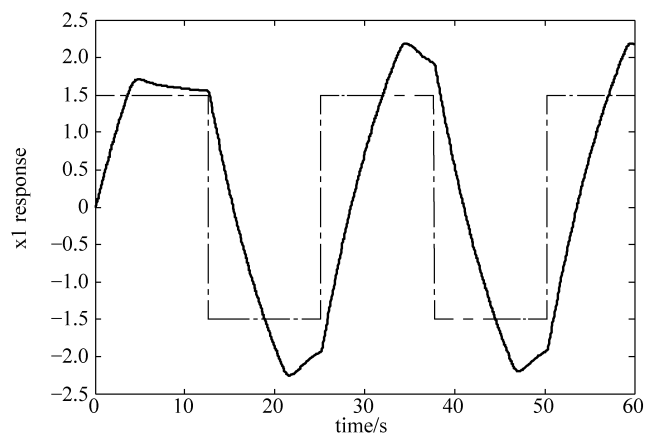


图 5.8 方波响应(不加补偿器)

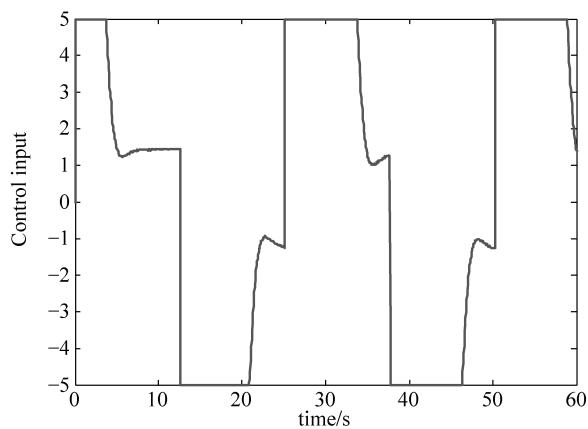


图 5.9 控制输入(不加补偿器)


```

nc = 3; % 控制器动态阶数
nu = 1; % 控制输入个数
nw = 2; % 外加输入个数
nz = 1; % 性能指标个数
naw = 0; % 补偿器状态阶数
ncl = np + nc;
nv = nu + nc;
npc = np + nc;
n = np + nc + naw;
m = ncl + nu + nw + nz;
% Plant defination
Ap = [0 1; -1 -10];
Bpu = [0;1];
Cpy = [1 0];
Dpyu = 0;

Bpw0 = Bpu;
Bpr = zeros(2,1);
Bpw = [Bpw0 Bpr];

Dpyw0 = 1;
Dpyr = 0;
Dpyw = [Dpyw0 Dpyr];
% error performance
Cpz = Cpy;
Dpzu = Dpyu;
Dpzw = Dpyw - [0 1];

% other performance
nx = 2; % 状态维数
ny = 1; % 输出维数
sys = ss(Ap, Bpu, Cpy, Dpyu);

% Used in lqi
Q = [5 0 0; 0 5 0; 0 0 60];
R1 = 0.001;
N = 0;
K = lqi(sys, Q, R1, N);
Kx = K(1:nx);
Ki = K(nx + 1:nx + ny);

Plant = ss(Ap, [Bpu Bpw0], Cpy, [Dpyu Dpyw0]);
Qn = 10; Rn = 10; Nn = 0;
[kalmf, L] = kalman(Plant, Qn, Rn, Nn);

Ac = [Ap - Bpu * Kx - L * Cpy + L * Dpyu * Kx - Bpu * Ki + L * Dpyu * Ki;
      zeros(ny, nx) zeros(ny, ny)];
Bcy = [L; - eye(ny)];
Bcwr = [zeros(nx, 1); eye(ny)];
Bcw = [zeros(3, 1) Bcwr];

```



```
% H1 = [Bclv' zeros(naw,nv)]; % naw = 0
H1 = Bclv';
H2 = Dcluv';
H3 = Dclzv';
H = [H1 H2 zeros(naw + nv,nw) H3];
% GU = [zeros(naw,nu + nw + nz);zeros(nu,n) eye(nu) zeros(nu,nw + nz)]; % naw = 0
GU = [zeros(nu,n) eye(nu) zeros(nu,nw + nz)];

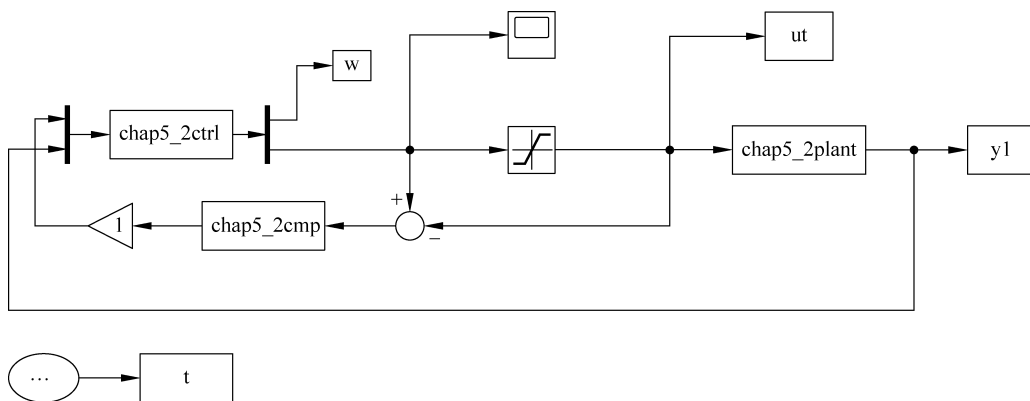
Mu = 0;
Stro = -2 * (1 - Mu) * U + (Dcluq * U + [zeros(nu,nc) eye(nu)] * Au) + (Dcluq * U +
[zeros(nu,nc) eye(nu)] * Au)';
Anti = fai + GU' * Au' * H + H' * Au * GU;

Fa = set(Stro < 0) + set(Anti < 0); % Second step, LMI to get Au and UU
solvesdp(Fa,ga);
gama = double(ga)
Au = double(Au);
UU = double(U);
Daw = Au * inv(UU)

Daw1 = Daw(1:2,:);
Daw2 = Daw(3,:);

save anti_file Daw;
```

(2) Simulink 主程序: chap5_2sim.mdl



(3) 控制器程序: chap5_2ctrl.m

```
% LQG controller with AW
function [sys,x0,str,ts] = s_function(t,x,u,flag)
switch flag,
case 0,
    [sys,x0,str,ts] = mdlInitializeSizes;
case 1,
    sys = mdlDerivatives(t,x,u);
case 3,
    sys = mdlOutputs(t,x,u);
```

```

case {1,2, 4, 9 }
    sys = [];
otherwise
    error(['Unhandled flag = ',num2str(flag)]);
end
function [sys,x0,str,ts]=mdlInitializeSizes
sizes = simsizes;
sizes.NumContStates = 3;
sizes.NumDiscStates = 0;
sizes.NumOutputs = 2;
sizes.NumInputs = 5;
sizes.DirFeedthrough = 1;
sizes.NumSampleTimes = 1;
sys=simsizes(sizes);
x0=[0 0 0];
str=[];
ts=[0 0];
function sys=mdlDerivatives(t,x,u)
w=1.5 * square(0.25 * t);
y=u(5);
v1=[u(1) u(2) u(3)]';

% From chap5_1LQG.m
Ac=[ -0.0081 1.0000 0; -203.8428 -74.1936 244.9490;
      0 0 0];
Bcy=[0.0081;0.5; -1];

Bcw=[0 0;
      0 0;
      0 1];
sys(1:3)=Ac * x + Bcy * y + Bcw(:,2) * w + v1;
function sys=mdlOutputs(t,x,u)
w=1.5 * square(0.25 * t);
v2=u(4);
y=u(5);
% From chap5_1LQG.m
Cc=[ -202.3428 -64.1936 244.9490];
Dcy=0;
Dcw=[0 0];

xc=[x(1) x(2) x(3)]';
ut=Cc * xc + Dcy * y + Dcw(:,2) * w + v2;

sys(1)=w;
sys(2)=ut;

```

(4) 补偿程序: chap5_2cmp.m

```

function [sys,x0,str,ts]=s_function(t,x,u,flag)
switch flag,
case 0,

```

```

        [sys,x0,str,ts] = mdlInitializeSizes;
    case 3,
        sys = mdlOutputs(t,x,u);
    case {2, 4, 9 }
        sys = [];
    otherwise
        error(['Unhandled flag = ',num2str(flag)]);
    end
function [sys,x0,str,ts] = mdlInitializeSizes
    sizes = simsizes;
    sizes.NumContStates = 0;
    sizes.NumDiscStates = 0;
    sizes.NumOutputs = 4;
    sizes.NumInputs = 1;
    sizes.DirFeedthrough = 1;
    sizes.NumSampleTimes = 0;
    sys = simsizes(sizes);
    x0 = [];
    str = [];
    ts = [];
    function sys = mdlOutputs(t,x,u)
persistent Daw
if t == 0
    load anti_file; % Daw
end
% Daw = [ 0.0038 -0.0395 -0.0118 0.9990];
q = u(1);
v = Daw * q;
sys(1:4) = v;

```

(5) 被控对象程序: chap5_2plant.m

```

function [sys,x0,str,ts] = s_function(t,x,u,flag)
switch flag,
case 0,
    [sys,x0,str,ts] = mdlInitializeSizes;
case 1,
    sys = mdlDerivatives(t,x,u);
case 3,
    sys = mdlOutputs(t,x,u);
case {2, 4, 9 }
    sys = [];
otherwise
    error(['Unhandled flag = ',num2str(flag)]);
end
function [sys,x0,str,ts] = mdlInitializeSizes
    sizes = simsizes;
    sizes.NumContStates = 2;
    sizes.NumDiscStates = 0;
    sizes.NumOutputs = 1;
    sizes.NumInputs = 1;

```

```

sizes.DirFeedthrough = 0;
sizes.NumSampleTimes = 1;
sys = simsizes(sizes);
x0 = [0 0];
str = [];
ts = [0 0];
function sys = mdlDerivatives(t,x,u)
ut = u(1);
wn = 0; % 0.001 * randn(1,100);
Ap = [0 1; -1 -10];
Bpu = [0;1];
Cpy = [1 0];
Dpyu = 0;
Bpw0 = Bpu;
sys(1:2) = Ap * x + Bpu * ut + Bpw0 * wn;
function sys = mdlOutputs(t,x,u)
Cpy = [1 0];
Dpyw0 = 1;
vn = 0; % 0.0001 * randn(1,100);
sys = Cpy * x + Dpyw0 * vn;      % th

```

(6) 作图程序: chap5_2plot.m

```

close all;

figure(1);
plot(t,w,'-r',t,y1,'k','linewidth',2);
xlabel('time(s)');ylabel('x1 response');

figure(2);
plot(t,ut(:,1),'r','linewidth',2);
xlabel('time(s)');ylabel('Control input');

```

参考文献

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- [2] Grimm G, Hatfield J, Postlethwaite I, et al. Antiwindup for stable linear systems with input saturation: an LMI-based synthesis[J]. IEEE Transactions on Automatic Control, 2003, 48(9): 1509-1525.
- [3] Ailon A. Simple tracking controllers for autonomous VTOL aircraft with bounded inputs[J]. IEEE Transactions on Automatic Control, 2010, 55(3): 737-743.
- [4] Wen C Y, Zhou J, Liu Z T, et al. Robust adaptive control of uncertain nonlinear systems in the presence of input saturation and external disturbance[J]. IEEE Transactions on Automatic Control, 2011, 56(7): 1672-1678.
- [5] Hu T S, Teel A, Zaccarian L. Stability and performance for saturated systems via quadratic and non-quadratic lyapunov functions[J]. IEEE Transactions on Automatic Control, 2006, 51(3): 1770-1786.